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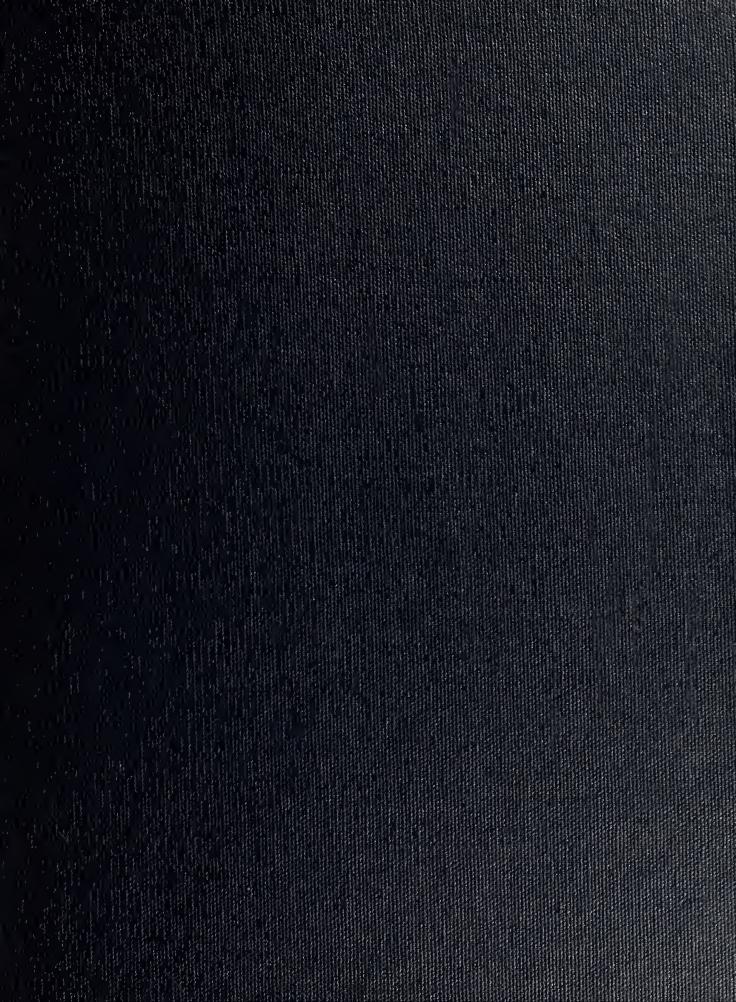
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# NAVAL POSTGRADUATE SCHOOL

Monterey, California



# THESIS

INTERACTIVE COMPUTER PROGRAM
FOR THE
ANALYSIS AND DESIGN OF LINEAR
TIME INVARIANT SYSTEMS

by

Habib Ismail December 1984

Thesis Advisor:

G. J. Thaler

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In this thesis, an interactive computer program for the analysis and design of time invariant unity feedback control systems is presented, using cascade or feedback or both types of compensation.

By using this program, the user is freed from the tedious, time consuming and error prone method of hand calculations, letting the computer handle these tasks

efficiently and speedily. The user can then concentrate fully on the placement of poles and zeroes of the compensator(s) used.

Design of control systems by classical methods being essentially a repetitive, trial and error procedure, this program greatly cuts down the turn around time and leads to faster, more satisfactory results.

2

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Interactive Computer Program
for the
Analysis and Design of Linear Time Invariant Systems

by

Habib Ismail Lieutenant Commander, Pakistan Navy B.E., University of Karachi, Pakistan, 1974

Submitted in partial fulfillment of the requirements for the degree of

MASTER OF SCIENCE IN ELECTRICAL ENGINEERING from the

NAVAL POSTGRADUATE SCHOOL December 1984 D' 27943

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#### I. INTRODUCTION

During the past two decades, the scientific and engineering communities have witnessed an ever increasing role of the digital computer in the fields of research, development and analysis of systems. The computer, today, is being used to solve engineering problems, whose solution, until very recently required long and tedious procedures. Still, it is probably true that this machine has potential not fully recognized yet, which is why the attention of so many computer scientists/engineers is focused on devising more efficient and innovative operating procedures.

Control system design is one area where classical theory has been extensively developed and used. It is fair to say that even today, most analysis and design problems of linear, time invariant control systems can still be approached using the methods developed by Bode, Nyquist and others.

A totally new approach to the design of control systems became available with the development of optimal control theory and the state variable analysis. These methods have been intensively developed in the last 10-15 years, but now their weaknesses have been exposed too. The "states" of the plant may not necessarily represent physically measurable quantities, and consequently it may not be possible to

implement the results at all. Luenberger's observers, designed to overcome this problem, can at best provide estimates of the state trajectory. Furthermore, the optimal control approach to design relies very heavily on mathematical manipulation, providing little insight to the actual working of the plant; the only input of the designer being the form of the cost function.

An intelligent use of the speed and information processing ability of the digital computer, coupled with the reliable features of classical theory appear to be the best solution to the problem at hand. The classical approach to design, being essentially a trial and error method, if the order of the system is fairly high, the number of repetitive calculations and the time required to perform these calculations becomes prohibitively large, the assistance of the computer in such problems becomes indispensable.

The work in this thesis was to develop an interactive, user oriented computer program that would prompt the user to input the transfer function and cascade/feedback compensators. The program would then display on the IBM 3277 - Tektronix 618 dial screen terminals the Bode Plot of both magnitude and phase. The program could be repeatedly used, with the user having the option to change/modify the compensators, each time viewing the effect of his modifications on the screen until he arrives at a satisfactory solution.

#### II. CONTROL ENGINEERING ANALYSIS

#### A. GENERAL

A continuous time control system may be represented in one of the following forms:

- a. Transfer functions
- b. State equations
- c. System block diagrams or signal flow graphs

Algorithms exist in almost every undergraduate control engineering text to convert the system representation from one given form to another. Gianniotis (Ref. 1) describes a simple method of converting from transfer function to state variable form in Chapter II.

The transfer function representation in its most general form is:

$$A_{m}S^{m} + A_{m-1}S^{m-1} + A_{m-2}S^{m-2} + \dots A_{o}S^{o}$$

$$B_{n}S^{n} + B_{n-1}S^{n-1} + B_{n-2}S^{n-2} + \dots B_{o}S^{o}$$

Usually the mathematical description of the system is found in the transfer function form in the literature.

Analysis and design of control systems by classical methods also requires the representation of the system in this form.

This thesis does not address the problem of converting from one form of representation to another. It is assumed that any conversions necessary have already been performed and that the system is represented by its open loop transfer function.

#### B. PROBLEM FORMULATION

Each system design has its own unique characteristics, but in general the system has to meet some kind of performance standards. These performance standards are generally provided as numerical specifications. The first step in the design of a control system is to analyze the system by itself in the usual feedback loop configuration. This is usually referred to as the uncompensated system.

Analysis of the uncompensated system almost always shows that the system cannot meet some or all of the given performance standards. Usually, additional components have to be inserted in the system for the purpose of altering the performance of the system. These components are called compensators. Compensation is a two step procedure, in which additional components (compensators) are inserted to change the structure of the system, and these components are then adjusted until the performance characteristics are satisfied.

The theory of cascade and feedback compensation is discussed in detail by Thaler (Ref. 2) in Chapters 5 and 6. Only a brief discussion of the types of compensators is presented here.

Compensators used in the design of feedback control systems are generally classified as shown in the block diagrams of figure 1.

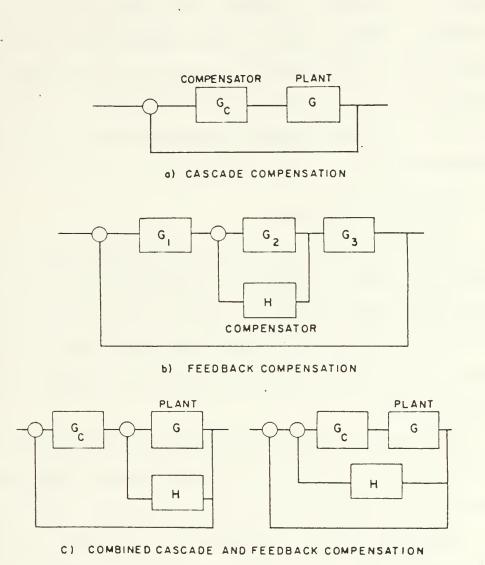


Figure 1. Classification of Compensation Structures

Cascade compensation may further be classified into two further types; a high pass filter usually called a phase lead compensator, and a low pass or phase lag compensator.

The selection of the type of compensator(s) to be used depends on a number of factors, the important ones being experience, personal preferences, availability, system constraints, etc. Unfortunately, there are no mathematical techniques to help in this selection process. Generally, one has to complete several designs and then choose the most appropriate one.

#### C. COMPUTER AIDED DESIGN

Of all the classical design methods available, the Bode diagram technique is generally considered to be the simplest, at the same time providing the most insight into system performance and behavior. The Bode design method may be used equally effectively both with cascade and feedback compensation schemes.

The computer program developed in this thesis displays on the terminal, initially, the Bode diagram (magnitude and phase) of the uncompensated open loop system. The user may then select the type of compensator to be used, and feed this information to the computer. The display changes, now showing the compensated system Bode Plot. This procedure may be repeated iteratively, with the computer updating the Bode Plot with each change made.

It was found on the average that turn around time for a typical third order system with two cascade compensators is less than five minutes.

#### III. PROGRAMMING CONSIDERATIONS

#### A. GENERAL

Any interactive software package, such as the one developed in this thesis must provide a simple yet unambigous means of data input and output. The data must be easy to interpret and apply to the problem at hand. Programs producing highly satisfactory results but requiring long studying time and/or special programming skills are of limited use only.

The intent of this thesis is to present such a program,

Computer Aided Design of Linear Systems. Special care has

been taken to develop the program so that the user has to

invest very little time learning to use it.

#### B. MAIN FEATURES OF THE PROGRAM

The development of a user oriented interactive computer program in solving engineering problems requires a considerable amount of programming work, contributing significantly to its complexity and size.

The computer program, hereafter referred to as BODPLT consists of a main program, a number of programmer-composed subroutines, a few library functions/subroutines, and various subroutines of the DISSPLA graphics package. The entire program is written in the FORTRAN IV language.

In brief, the whole BODPLT package works as follows:

A user, logged into the VM/CMS environment of the system from the dual screen terminals, issues the command DISSPLA BODPLT.

The package then assumes control. The program begins its execution by interrogating the user and calling the appropriate subroutine accordingly. All programmer-composed subprograms are included in the main program titled BODPLT FORTRAN.

The BODPLT program has the following important features:

- runs of the VM/CMS time sharing system.
- interrogates the user in entering all problem specifications from the terminal.
- can handle up to a ninth order plant transfer function, six first order and one second order cascade filters.
- prompts the user to input the parameters of velocity feedback, acceleration feedback or approximate acceleration feedback as required.
- provides the solution in tabular form on the IBM 3277 screen and the Bode Plot on the TEK 618 terminal.
- can provide hard copy version of the problem specifications and tabular output by using the RECORD ON/RECORD OFF execs, and of the BODE PLOT on the Tektronix printer where installed.
- allows problem specifications to be changed between runs.

#### C. PROGRAM DESCRIPTION

The main program is the coordination center which controls the calling of the supporting subroutines, in order to input the transfer function, cascade/feedback compensators and other necessary information. The tabular results and the Bode Plot are then displayed on the two screens respectively.

The main program as well as the accompanying subroutines can be found in Appendix A. They contain a sufficient number of comment cards to be self explanatory.

The following is a brief description of the performance and purpose of the various subroutines.

NUMER inputs the numerator of the plant transfer function.

<u>DENOM</u> inputs the denominator of the plant transfer function.

CASCAD inputs up to 6 first order lead/lag filters.

SECAS inputs the numerator of the second order band pass/band stop filter.

SECASD inputs the denominator of the second order filter.

 $\underline{\text{FETCH}}$  determines the value of the radial frequency, w, at the origin of the x-axis.

<u>DECADE</u> determines the number of decades of frequency to be spanned.

FEEDBK inputs the various parameters of feedback compensators.

TITLES inputs the two lines of text as headings for the Bode Plot.

In addition, the main program handles the tasks of displaying the tabular output and the Bode Plot of the open and closed loop response of the system as required.

#### IV. PROGRAM PERFORMANCE INVESTIGATION

#### A. GENERAL

The program was tested by solving several linear control system design problems. Very satisfactory results were obtained in all cases with remarkable efficiency and speed. The only necessary condition is proper problem formulation. This is true for any interactive computer program. Once the program is used a couple of times, the user gets the necessary familiarity with its working.

The example problems presented below are used to demonstrate the performance and capabilities of the program. The examples can also help the user in formulating his own particular problem. The examples were selected from Thaler's 'Design of Feedback Systems' (Ref. 2)

#### B. EXAMPLE PROBLEMS

#### 1. Example 4.1 : A Phase Lead Network

#### a. Problem Statement

A positioning system is single loop with unity feedback and forward transfer function

$$G(s) = \frac{5.0}{s(0.7s + 1)(0.3s + 1)}$$

The velocity constant is not to be decreased. Design a phase lead compensator which will provide  $M_{\mbox{\scriptsize pW}}$  less than 1.5.

#### b. Solution

The first step is to get the transfer function in the required form:

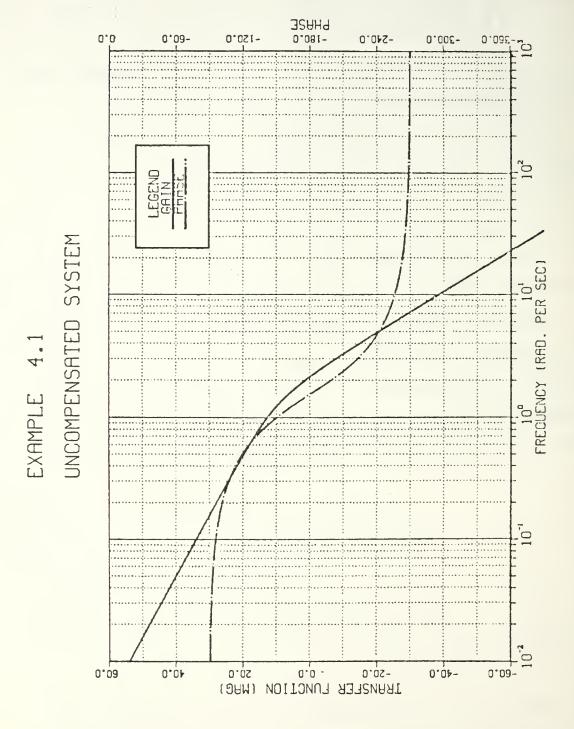
$$G(s) = \frac{5.0}{0.21s^3 + 1.0s^2 + 1.0s}$$
 (4.2)

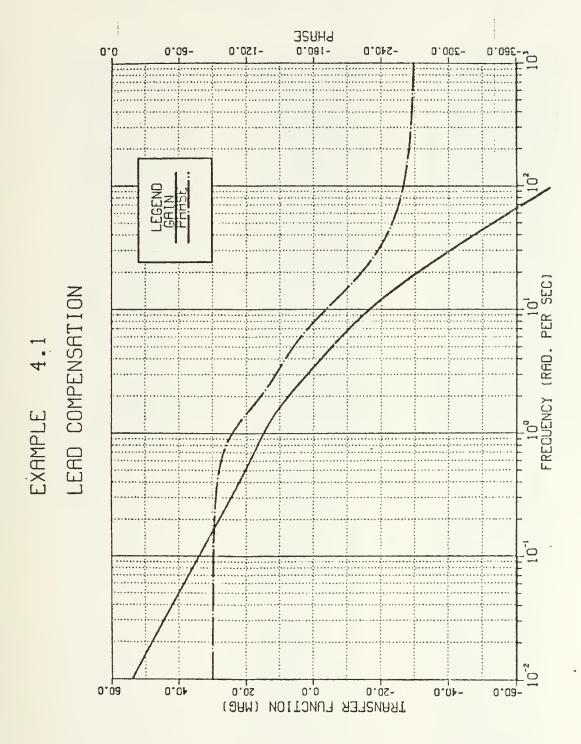
The Bode Plot of the uncompensated system drawn using the program is shown on figure 2 and the tabular output on table 1. The uncompensated system has a phase margin of -20 degrees. To achieve a M<sub>pw</sub> of less than 1.5, a phase margin of 44 degrees or more is required. Approximately 64 degrees of positive phase shift are therefore needed. Two sections of lead filter are introduced as given below:

$$G_{C} = \frac{(S/3.0 + 1) (S/1.5 + 1)}{(S/10.0 + 1)^{2}}$$

The compensated Bode Plot is given on figure 3 showing a phase margin of 35 degrees.

It may be pointed out that the final values for the lead filter poles and zeroes were arrived at after 3 iterations and this design problem was solved in less than 15 minutes.

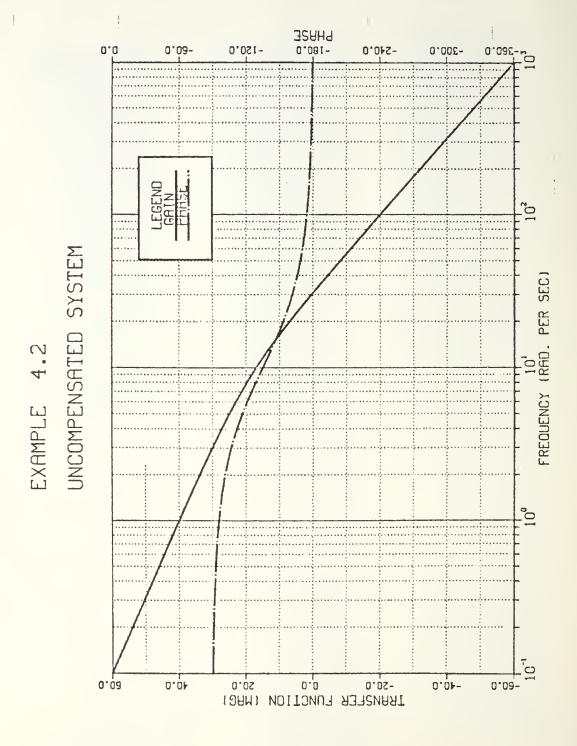




Lead Compensation Bode Plot of Example 4.1 Figure

# Table 1. (Contd.)

0.514174E+01	0.464157E+C1	-0.480013E+01	-0.100608E+03
0.569579E+01	0.514174E+01	-0.636283E+01	-0.163974E+03
0.693945E+01		-0.788934E+01	-0.107576E+03
0.774261E+01	0.630955E+C1	-0.944966E+01	-0.171432E+U3
0.857692E+01	0.093945E+01	-0.110539E+02	-0.17554UE+Ua
0.950116E+01	0.774261E+01	-0.127116E+02	-0.179883E+03
0.105250E+02	0.857694E+01	-0.144313E+02	-0.184433E+03
0.115591E+02	0.950116E+01	-0.162196E+02	-0.189133E+03
0.129155E+02	U.105250E+02	-0.180814E+02	-U.193936E+U3
0.145 072 E + 02	0.115591E+02		-0.198782E+03
0.158489E+02	0.129155E+02	-0.220340E+02	-0.203012E+03
0.175567E+02	0.143072E+02	-0.241236E+02	-0.208369E+U3
0.194485E+02	0.158489E+02	-0.262850E+02°	-0.213003E+03
0.215443E+02	0.175567E+02	-0.285134E+04	-0.217469E+03
0.238658E+62       -0.355431E+02       -0.229574E+03         0.264375E+02       -0.379807E+02       -0.233121E+03         0.292863E+02       -0.404556E+02       -0.239416E+03         0.359380E+02       -0.429023E+02       -0.239402E+03         0.398106E+02       -0.454962E+02       -0.24267E+03         0.441004E+02       -0.506288E+02       -0.247195E+03         0.44104E+02       -0.532208E+02       -0.249344E+03         0.541167E+02       -0.532208E+02       -0.249344E+03         0.599483E+02       -0.584423E+02       -0.253083E+03         0.664080E+02       -0.610677E+02       -0.254700E+03         0.314910E+02       -0.637005E+02       -0.257498E+03         0.902722E+02       -0.689835E+02       -0.258703E+03	0 .194485E+02	-0.308033E+02	-0.221735E+03
0.264375E+02	0.215443E+02	-0.331486E+02	-0.225776E+03
0.292863E+02		-0.355431E+02	-0.2295 <b>7</b> 4E+03
0.324421E+02	0.264375E+02	-U.379807E+02	-0.233121E+03
0.359380E+02	0.292863E+02	00.00.000.00	-0.236416E+03
0.398106E+02	0 0000 000	-0.429023E+02	-0.239462E+03
0.441004E+02       -0.506288E+02       -0.247195E+03         0.488526E+02       -0.532208E+02       -0.249344E+03         0.541167E+02       -0.558260E+02       -0.251302E+03         0.599483E+02       -0.584423E+02       -0.253083E+03         0.664080E+02       -0.610677E+02       -0.254700E+03         0.735639E+02       -0.657005E+02       -0.257498E+03         0.902722E+02       -0.689835E+02       -0.258703E+03	0.359380E+02	-0.454962E+02	-0.242267E+05
0.488526E+02       -0.532208E+02       -0.249344E+03         0.541167E+02       -0.558260E+02       -0.251302E+03         0.599483E+02       -0.584423E+02       -0.253083E+03         0.664080E+02       -0.610677E+02       -0.254700E+03         0.735639E+02       -0.657005E+02       -0.257498E+03         0.814910E+02       -0.663395E+02       -0.257498E+03         0.902722E+02       -0.689835E+02       -0.258703E+03	0.398106E+02		-0.244840E+03
0.541 167E+02       -0.558260E+02       -0.251302E+03         0.599483E+02       -0.584423E+02       -0.253083E+03         0.664080E+02       -0.610677E+02       -0.254700E+03         0.735639E+02       -0.657005E+02       -0.257498E+03         0.902722E+02       -0.689835E+02       -0.258703E+03	0 1 1 1 2 0 0 1 2 0 2		-0.247195E+05
0.599483E+02	00.003202 02	0.3322002.02	002.73.12.03
0.664080E+02			
0.735639E+02			
0.814910.E+02		00 0 2 0 0 1 1 2 1 0 2	
0.902722E+02 -0.689835E+02 -0.258703E+03	4 4 1 2 2 2 2 2 2	010010050	
010000000000000000000000000000000000000			000000
0.999998E+02 -0.716317E+02 -0.259793E+03	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		77230.032.03
	0.9999986+02	-0.716317E+02	-0.259793E+03



PHASE 10' FREGUENCY (RAD. PER SEC) EXAMPLE 4.2 LAG/LEAD COMP. 0.01 0.0 0.08 o.os 0.02-0.01-0.09-IRANSFER FUNCTION (MAG)

Figure 5. Lag/Lead Compensation in Example 4.2

U.100000E+00 0.590345E+02 0.1127712E+03 0.122712E+03 0.125712E+03 0.135935E+03 0.135935E+03 0.135935E+03 0.135935E+03 0.150384E+03 0.204697E+03 0.204697E+03 0.204697E+03 0.204697E+03 0.204697E+03 0.204697E+03 0.204697E+03 0.204697E+03 0.204697E+03 0.211274E+03 0.278256E+03 0.211274E+03 0.278256E+03 0.241454E+03 0.278256E+03 0.341454E+03 0.341454E+03 0.4419008E+03 0.341458E+03 0.4419008E+03 0.441908E+03 0.	0.112776E+00 0.589089E+02 0.1127712E+C0 0.579754E+02 0.112769E+03 0.150534E+00 0.560783E+02 0.1005058E+03 0.160810E+00 0.560783E+02 0.1005058E+03 0.160810E+00 0.551106E+02 0.1005058E+03 0.204697E+00 0.551106E+02 0.204697E+00 0.551126E+02 0.1105331E+03 0.224754E+00 0.551126E+02 0.21012E+02 0.110333E+03 0.2251188E+00 0.510529E+02 0.1112174E+03 0.308240E+00 0.499765E+02 0.311217E+03 0.341454E+00 0.464158E+00 0.464158E+00 0.464158E+00 0.440098E+02 0.514175E+00 0.569560.E+00 0.569560.E+00 0.569560.E+00 0.51252E+02 0.5132106E+03 0.50308946E+00 0.5132106E+02 0.5144175E+00 0.569560.E+00 0.5132106E+02 0.5144175E+00 0.569560.E+00 0.5132106E+02 0.5132106E+03 0.598946E+00 0.33785E+02 0.112491E+03 0.598946E+01 0.3387765E+02 0.1132106E+03 0.75695E+01 0.3377155E+02 0.133500E+03 0.105250E+01 0.3377155E+02 0.1336457E+03 0.116591E+01 0.336350E+02 0.1336356E+02 0.1336457E+03 0.116591E+01 0.327090E+02 0.135758E+03 0.143072E+01 0.2664375E+01 0.22664375E+01 0.22664375E+01 0.22664375E+01 0.23665E+02 0.124695E+03 0.34858E+01 0.264375E+01 0.292864E+01 0.168860E+02 0.112606E+03 0.34940E+01 0.292864E+01 0.168860E+02 0.1126069E+03 0.292864E+01 0.168860E+02 0.1126069E+03 0.34940E+01 0.21664375E+01 0.2166498E+02 0.1126969E+03 0.34940E+01 0.21664375E+01 0.226164E+02 0.1126969E+03 0.34940E+01 0.248658E+01 0.248668E+01 0.248668E+
0.378247E+02 $-0.905738E+01$ $-0.130883E+03$	0.999999E+01 0.10775E+02 0.122712E+C2 0.155935E+02 0.150583E+02 0.166858E+00 0.166809E+02 0.184734E+02 0.204696E+02 0.205011E+01 0.166809E+01 0.166809E+02 0.134252E+01 0.204696E+02 0.236847E+01 0.219201E+03 0.251188E+02 0.276255E+02 0.276255E+02 0.308239E+02 0.341454E+02 0.3485960E+01 0.119201E+03 0.276255E+02 0.3785960E+01 0.1126281E+03 0.344454E+02 0.785960E+01 0.1126281E+03

# Table 2. (Contd.)

0.464157E+C2 0.514174c+C2	-0.115780E+02 -0.129043E+02	-0.135950E+03
0.569579E+02	-0.142753E+02	-0.141232E+03
0.630955E+C2 0.698945E+02	-0.156905E+02 -0.171484E+02	-0.143871E+03
0.036343E+02	-0.186466E+02	-0.148993E+03
0.857692E+02	-0.201822E+02	-0.151427E+03
0.950116E+02 0.105250E+C3	-0.217522E+02 -0.233528E+02	-0.153749E+03
0.1105918+03	-0.233320E+02	-C.158014E+03
0.129155E+03	-0.266322E+02	-0.159944E+03
0.143072E+C3 0.158489E+C3	-C. 283043E+02 -0.299941E+02	-0.101730E+03 -0.163392E+03
0.175567E+03	-0.310988E+02	-0.164917E+03
0.194485E+C3	-0.334161E+02	-C.100210E+02
0.215443E+03 0.238658E+C3	-0.351439E+02 -0.368805E+02	-C.167597E+U3
0.264375E+C3	-0.386245E+02	-C.169830E+03
0.292863E+03	-0.403745E+02	-0.170798E+03
0.324421E+C3 0.359380E+C3	-0.421296E+02 -0.438888E+02	-0.171678E+03
0.3981C5E+C3	-0.456513E+UZ	-0.173199E+03
0.441 CC4E+C3	-0.474166E+02	-0.173854E+03
0.4885∠5E+03 0.541167E+01	-0.491842E+02 -0.509536E+02	-C.174447E+03
0.599482E+C3	-0.527247E+02	-C.175469E+03
0.664 080 E+03	-0.544969E+02	-0.175907E+03
0.735639E+C3 0.8149.0E+03	-0.562762E+02 -0.580443E+02	-0.176304E+03
0.902721E+03	-0.598190E+02	-0.176986E+U3
0.999998E+03	-C. 615944E+02	-C.177278E+03

## 3. Example 4.3 : Velocity Feedback

#### a. Problem Statement

A simple second-order servo is to be compensated with tachometer feedback. The forward transfer function is

$$G(S) = \frac{100.0}{S(S + 1)}$$

and the tachometer transfer function is  $K_tS$ . The tachometer is fed back around <u>all</u> of the forward gain. Using Bode diagram methods, set  $K_t$  to provide  $M_{pw} = 1.3$ .

#### b. Solution

Bode Plot for this system is shown on figure 6. The system has a phase margin of about 6 degrees. For  $M_{pw} = 1.3$ , a phase margin of 45 degrees is required. A rough graphical design on the uncompensated Bode Plot gives

$$1/H = 12.0/S$$
 or  $H = 0.08S$ 

The Bode Plot for the compensated system is on figure 7, showing a phase margin of 50 degrees.

The close loop frequency response of this example, drawn using BODPLT is shown on figure 8.

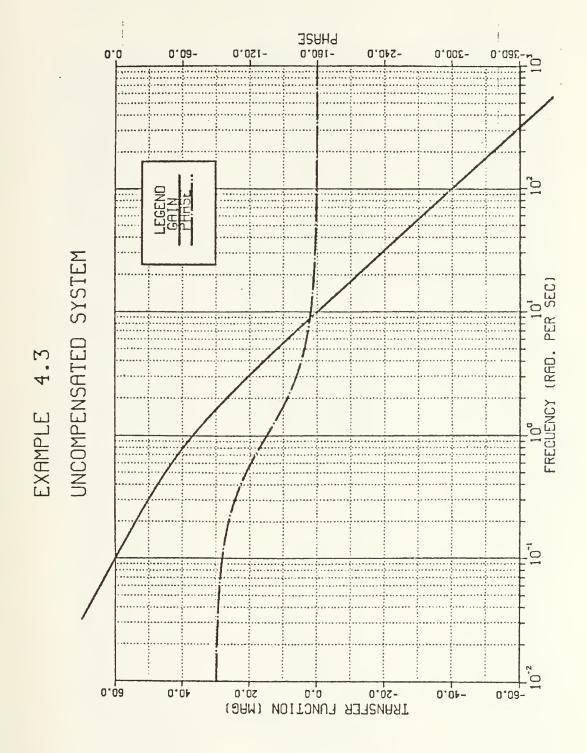
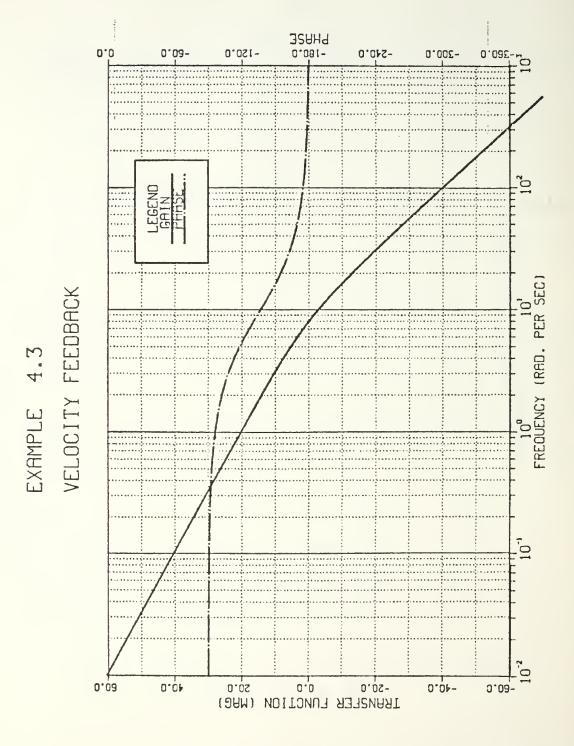


Figure 6. Uncompensated Bode Plot of Example 4.3



33

Table 3. Tabular Output of Example 4.3

FREW	MAGNITUDE	PHASE
0.103646E-C1 0.129155E-C1 0.146780E-C1 0.146780E-C1 0.146780E-C1 0.14673E-C1 0.189573E-C1 0.244843E-C1 0.27824E-C1 0.278248E-C1 0.278248E-C0 0.359381E-C0 0.4684293E-C0 0.527493E-C0 0.527493E-C0 0.527493E-C0 0.527493E-C0 0.527493E-C0 0.527493E-C0 0.527493E-C0 0.129155E+C0 0.129155E+C0 0.129155E+C0 0.129155E+C1 0.13646E+C1 0.129155E+C1 0.13646E+C1 0.129155E+C1 0.13646E+C1 0.129155E+C1 0.12915E+C1 0.12915E+C1 0.12915E+C1 0.12915E+C1 0.12915E+C1 0.12915E+C1	0.6395.498.65E+022 0.5584081E+022 0.5584081E+022 0.5584081E+022 0.5584081E+022 0.5584081E+022 0.5584081E+022 0.5539632E+022 0.5517413EE+022 0.5517413EE+022 0.5517413EE+022 0.5517413EE+022 0.5498498EE+022 0.4472886EE+022 0.4472886EE+022 0.447385EE+022 0.447385EE+022 0.428862E+022 0.428862E+022 0.428862E+022 0.428862E+022 0.3387418EE+022 0.428862EE+022 0.33849862EE+022 0.33874862EE+022 0.33874862EE+022 0.33874862EE+022 0.3398498EE+022 0.33988EE+022 0.33988EE+022 0.33988EE+022 0.33988EE+022 0.33988EE+022 0.33988EE+022 0.33988EE+022 0.33988EE+022 0.33988EE+022 0.33988EE+022 0.33988EE+022 0.33988EE+022 0.339888EE+022 0.33988EE+022 0.339888EE+022 0.339888EE+022 0.339888EE+022 0.339888EE+022 0.339888EE+022 0.339888EE+022 0.339888EE+022 0.339888EE+022 0.339888EE+022 0.339888EE+022 0.339888EE+022 0.339888EE+022 0.339888EE+022 0.3398888EE+022 0.3398	-C.900784E+0022-022-0900784E+0022-0900784E+0022-022-09007894E+0022-022-09007894E+0022-022-090078-033E+0022-090078-033E+0022-0900797948EE+0022-090079907948-033-06-9900799478-09090799478-09090998-00-990794-03-0-0-99079478-0-0-990794-0-0-9907974-0-0-990794-0-0-990795

# Table 3. (Contd.)

0.215443E+02	-0.140753E+02	-C.156650E+03
0.244843E+C2	-0.161408E+02	-0.159199E+03
0.278255E+C2	-0.182376E+02	-C.161517E+03
0.316226E+02	-0.203602E+02	-C.103009E+03
0.359380E+C2	-0.225037E+02	-0.105489E+03
0.408423E+02	-0.246639E+02	-C.107170E+03
0.404157E+C2	-0.268375E+02	-0.108668E+03
0.527497E+C2	- C. 290217E+02	-0.169999E+03
0.599482E+02	-0.312143E+02	-0.171179E+03
0.681290E+G2	-0.334134E+02	-0.172224E+03
0.774261E+02	-C.35p177E+02	-6.173148E+63
0.879919E+02	-0.378259E+02	-C.173964E+03
0.999995E+02	-0.400373E+02	-C.174084E+03
0.113646E+03	-0.422511E+02	-C.175319E+03
0.129154E+03	-0.444968E+02	-0.175079E+03
0.146779E+C3	-0.466840E+02	-0.176372E+03
0.166809E+03	-0.489023E+02	-0.176806E+03
0.189573E+C3	-0.511215E+02	-0.177189E+03
0.215443E+C3	-0.533413E+02	-0.177526E+03
0.244843E+O3	-0.555617E+02	-0.177822E+03
0.278255E+C3	-0.577825E+02	-0.178083E+03
0.310226E+C3	-0.600037E+02	-0.178313E+03
0.359379E+C3	-0.622250E+02	-0.178515E+03
0.408422E+C3	-0.644466E+02	-0.178693E+03
0.464157E+03	-0.66683E+02	-0.178650E+03
0.527497E+03	-0.688902E+02	-0.178688E+03
0.599481E+C3	-0.711121E+02	- (.179109E+03
0.681290E+03	-0.733341E+02	- (.179215E+03
0.774260E+C3	-0.755561E+02	- (.179309E+03
0.879918E+C3	-0.777782E+02	-C.179392E+U3
0.999957E+C3	-0.800003E+02	-O.179465E+O3

0.0 0.03--150°0 0.005-0.015-EXAMPLE 4.3 CLOSED LOOP RESPONSE 10' FREQUENCY (RAD. PER SEC) 0.02 0.09 0.01 0.0 0.05-0.01-0.09-TRANSFER FUNCTION (MAG)

**PHASE** 

Figure 8. Closed Loop Response of Example 4.3

#### V. CONCLUSION AND RECOMMENDATIONS

#### A. CONCLUSION

The objective of this thesis was to develop an interactive user oriented computer program which would aid in solving control engineering problems using the Bode method of design. The presented program proves that frequency domain design of control systems using the digital computer as an aid is not only feasible but highly desirable. The results obtained are readily interpretable and provide good and meaningful insight into the problem.

The results obtained during the investigation of the program performance show that a complicated but well formulated problem can be solved with ease, and the solution is obtained with speed, accuracy and precision.

The entire program is less than 1000 lines, with a total of 9 subroutines. Every effort has been made to keep the program simple yet unambigous, so that the user has to invest very little time learning how to use it. Effort has also been made to minimize the use of the computer CPU time. However, expenditure of CPU time is to a large measure dependent upon:

- (1) the order of the system.
- (2) the number of iterations used in reaching a solution.

(3) the type and order of the compensator(s) used.

#### B. RECOMMENDATIONS

The program as presented in this thesis seems to be able to adequately satisfy the usual needs in a control system design problem. A number of useful extensions to the work developed in this thesis can be carried out. These are briefly discussed.

#### 1. Curve Fitting

Although not specifically worked on in this thesis, the program can be used quite effectively for curve fitting purposes. This was demonstrated in the initial stages of the development of this program. The procedure is, by its very nature, iterative and therefore time consuming and cumbersome. However, the entire algorithm can be automated using a minimization subroutine, with the program outputting a polynomial to fit a given curve over a specified range of the independent variable.

## 2. Computer Selection of Compensators

A suitable minimization routine such as Box PLX can be incorporated into the program which could select the best possible location of poles and zeroes to meet given performance specifications. This would automate the entire Bode design procedure, the user then having the option of only specifying the type of compensation, i.e., cascade or feedback. It may however be pointed out that minimization

routines by the very nature of their operation are very time consuming and wasteful of CPU resources.

### 3. Root Locus

Most of the subroutines developed in this thesis are very general in nature and can be adapted quite easily to develop a similar interactive program for Root Locus plots.

## 4. Integrated Control System Design

No meaningful design of control systems is complete without finally analyzing its time domain performance. It is therefore considered highly desirable to incorporate into this program, an interactive Root Locus design procedure and then a time domain analysis of the compensated system. The entire package would then be an excellent teaching aid for control system design.

# APPENDIX PROGRAM LISTING

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(NA)
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K = J+1

WRITE(6,354) J,NA(K

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WRITE(6,355)

READ(5,279) ANSWER

IF (ANSWER, EQ.YES)
                                                                        DO 30 1 1=1,10
NA (1) = C.0
CONTINUE
CALL FRICMS(*CLRSCI
WRITE(6,351)
READ(5,374)NN
READ(5,377)ANSWER
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DA(I) = 0.0
CONTINUE
CALL FRICMS("CLRSCRN")
WRITE(6,451)
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MRITE(6,460)

DO 406 I=1.N

J= I-1

MRITE (6,453)

RE AD (5,478;END = 405)

GO TO 4C6

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CALL FRICMS ("CLRSCRN")

CONTINUE

CALL FRICMS ("CLRSCRN")

DU 407 I = 1.N
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K = J+1

WRITE(6,454) J,DA(K

CONTINCE

WRITE(6,455)

REAC(5,479) ANSWER

IF (ANSWER-EQ.YES)
SUBROUTINE
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DATA YES/*Y',
DO 520 I = 1.0
CZS.[1] = 1.0
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CONTINUE
CALL FRICMS("CLRSCRN")
WRITE(6,551)
READ(5,571)ANSWER
IF (ANSWER EQ. YES)CO TO 5
CONTINUE
CALL FRICMS("CLRSCRN")
READ(5,577)ANSWER
IF (ANSWER EQ. YES)CO TO 5
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WRITE (6,500)

DO 506 1=1,N

READ (5,578,END = 505) C2

GO TO 506

CALL FRICMS ("CLRSCRN")

WRITE (5,556)

GO TO 507

CONTINUE

CALL FRICMS ("CLRSCRN")

WRITE (6,554) I,CZS (I)

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RE AD (5,578,END = 515)

CALL FRICMS ("CLRSCRN")

WRITE (5,556)

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CONTINUE
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WRITE (6,557)

WRITE (6,555)

RE AD (5,577) ANSWER

IF (ANSWER EQ YES)

CONTINUE
CALL FRICMS ("CLRSCRN")

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50 306 1=1,3
51-1
50 NIN LE
WRITE (6,353) J
RE AD (5,378,END = 305) C
GU TO 3C
RE MIND 5
CALL FRICMS (*CLRSCRN*)
60 TO 304
CONTIN LE
CALL FRICMS(*CLRSCRN*)
DO 307 I = 1,3
                                                                                                                                                                                                                                                          J = 3-1

WRITE(6,354) J,CN(K)

CONTINCE

WRITE(6,355)

READ(5,379) ANSWER

IF (ANSWER.EQ.YES) GO TO

CONTINCE

CALL FRICMS (*CLRSCRN*)
                                                                                                              CALL FRICMS ("CLRSCRN")
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                                                                                                                      CALL FRICMS("CLRSCRN")
CONTINUE
WRITE(6,451)
DO 406 I=1,3
J=I-1
WRITE (6,453)
RE AD (5,478,END = 405) CL
GO TO 406
CALL FRICMS ("CLRSCRN")
MRITE(5,456)
                                                                                                                                                                                                                                                        K = J+1

WRITE(6,454) J,CD(K)

CCNTINCE

WRITE(6,455)

READ(5,479)ANSWER

IF (ANSWER.EQ.YES) GO 1

CONTINCE

CALL FRICMS("CLRS CRN")

RETURN
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CALL FRICMS ("CLRSCRN")
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AS FOLLOWS: '//,26X," FOR EXAMPLE '//,6X,"

IF LOWER LIMIT IS 10**(-02), ENTER -02',/',8X,"

IF LOWER LIMIT IS 10**(+11), ENTER +11',

FORMAT(//,7X," YOU HAVE PRESSED "ENTER" WITHOUT ENTERING ANY

NUMBER ",//,7X," TRY AGAIN.")

CORRECT? (Y/N):)
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INTEGER FENCM, YES, ANSWER
DATA YES/'Y'/
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                                                                             CONTINUE WRITE (6,51)
READ (5,16,END = 02) FEN CALL FRICMS (°CLRSCRN°)
GU TO C3
REWIND 5 CALL FRICMS (°CLRSCRN°)
REWIND 5 CALL FRICMS (°CLRSCRN°)
REITE (6,52) FENUM READ (5,77) ANSWER IF (ANSWER-EQ.YES) GO TO C1
CONTINUE REITERN
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                                             VARIABLE DECLARATIONS
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A YES/'Y.'/
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WRITE (6,151)
READ (5,176,END=102)DEC
CALL FRICMS (°CLRS CRN°)
GU TO 1G3
REWIND 5
CALL FRTCMS (°CLRS CRN°)
WRITE (6,152)
GUNTINUE
WRITE (6,153)DEC
WRITE (6,153)DEC
READ (5,177)ANSWER
IF (AN SKËR-EC-YES) GO TO 1
CONTINUE
RETURN
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                                                                 INTEGER TTL1, MSS1
DIMENSICN TTL1(5), MSS1(5)
WRITE(6,651)
RE AD(5,676) TTL1(1), TTL1(2), TTL1(5), TTL1(4), TTL1(5)
WRITE(6,653)
RE AD(5,676) MSS1(1), MSS1(2), MSS1(3), MSS1(4), MSS1(5)
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\*\*\*\* DATA MSS(1), MSS(2), MSS(4), MSS(5)/° °, WRITE(6,1072)

CONTINUE

DO 1005 I = 1.6

CZ(I) = 1.0

CZ(I) = 1.0 \* \* \* \* \*\*\*\*\* · 安本安安 安市安安安安安安安安安安安安安安安安安安安安安安安安安安安安安 中安安安安安 **神神神神神神神** VARIABLES SUBROUTINES CALL DENCM (B)
WRITE(6,1052)
READ(5,1C77)ANSWER
IF(.NCT.ANSWER.EQ.YES) GU TO 1001
CALL CASCAC(CZ,CP)
CONTINUE
WRITE(6,1056)
READ(5,1C77)ANSWER
IF(.NOT.ANSWER.EQ.YES)GU TO 1002 1001 ш PROGRAM INITIALIZ EQUIRED MAIN AND THE DECLARE  $\propto$ CALL 大安 安 安 大 **∱**Þ 计计计中 \* \* 净护 神林 \* \* \* 1100 2 1001 00000000 COC

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CALL SE(ASC(DI)

CALL SE(ASC(CDI)

RRITE(6,1060)

READ(5,167)ANSHER

IF(.NCT.ANSHER.EQ.YES.)GG TG 1015

CALL FECEK(FK,FN,CN,FF)

CALL FILES(TTL,MSS)

CALL TILLES(TTL,MSS)

CALL TILLES(TTL,MSS)

CONTINUE

ADECS = FLGAT(DECS)

WRITE(6,107C)

READ(5,107C)

FREC(II) = (10.0**(LCGh(I)))*(10.**(NUM))
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************ FEDBACK COMPENSATION *******
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IF (ANS2 . 6q . UPEN) GU TO 1128

H = HP (1.0 + (FP))

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YL=6.-.5-YW-.1
CALL BLNK1(XL-.3,8.-.4,YL-.3,6.-.4,2)
CALL LINESP(3.5)
SECFIL=NCAS2/DCAS2
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PHASE\$ ",-100,9.0,0.1 1006 Q. HMAG, 271, 01 60.,50.,0.,5., 0.9 CALL GRID(1,2)
CALL RESET('D3T')
CALL LEGLIN
CALL CURVE(FREQ'HWAG,271,0)
CALL VGRAXS (-360.,50.,0.,5)
CALL UBCL IN
CALL URVE(FREQ'PHASE,271,0)
CALL RESET('BLNK1')
CALL RESET('BLNK1')
CALL RESET('THKCR'')
CALL LEGEND(IPAK,2'XL'YL)
CALL LEGEND(IPAK,2'XL'YL)
CALL LEGEND(1)
WRITE(6,1051)
READ(5,1076)
READ(5,1076) CDNIINUE
WRITE(6:1053)
READ (5:1070)ANS
CALL FRICMS("CLRSCRN")
IF (ANS.ED.CHP)GD TO 1010
IF (ANS.ED.CHW)GO TO 1012
IF (ANS.ED.CHN)GO TO 1012
IF (ANS.ED.CHN)GO TO 1125
CALL DECADE(DECS)
COLL FICH (NUM)
COLL TITLES(TTL.MSS)
COLL DENUM(B)
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CALL FEEDUK(FK, FN, D.FP)
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#### LIST OF REFERENCES

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